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1 Amendments to the Specification:

2 Field of the invention

3 The present invention relates to the field of ink-
4 drop generators used in inkjet printers. It also relates
5 to a print head and a printer using said ink-drop
6 generator.

7 Background art

8 The principle of the inkjet printer is now well-
9 known and has been described, for example, in the
10 American patent No. US 3 373 437 granted to Richard G.
11 Sweet. In this type of printer an ink-drop generator
12 produces drops of ink that are electrically charged then
13 deflected or not deflected by deflecting electrodes to
14 print or not print a downstream substrate. The technology
15 of deflected continuous jets has been widely used in
16 industrial marking applications where inks incorporate
17 volatile solvents and/or pigments for mediums that are
18 difficult to mark where the atmosphere is rendered
19 difficult due to the presence of dust and a variable
20 temperature. The printed widths are small and the outputs
21 are high. A generator of small drops, such as that
described in French patent No. FR 2 653 063 (granted to

1 the present applicant), generally comprises a single
2 inkjet created from a pressurized inkjet cavity that has
3 a jet nozzle on one of its surfaces.

4 The ink cavity also has an elongated cylindrical
5 transducer on a surface opposite that which comprises the
6 nozzle. Said transducer vibrates at a high frequency
7 according to a longitudinal mode and constantly fragments
8 the jet into regular, identical, equidistant droplets.
9 The assembly consisting of the ink cavity, transducer and
10 nozzle plate is called an ink-drop generator. The ink-
11 drop generator is associated with charge electrodes,
12 deflecting electrodes and possibly an ink collector to
13 constitute a print head. One or more print heads can be
14 mounted on the same printer. One or more ink-drop
15 generators can also be assembled to constitute a single
16 print head. For instance, patent application No. 2 653
17 063 referred to above discloses a print head comprising
18 at least two modulation bodies and therefore at least two
19 nozzles equipped with means for adjusting each jet and a
20 single ink-collector module with a single pipe for
21 returning the ink to the common circuit. This type of
22 print head offers the possibility of printing large
23 characters at a higher rate than that provided by a head

1 with only one jet. The detailed embodiment of the
2 invention described below also comprises two modulation
3 bodies, which are also called acoustic-wave generators,
4 shakers, resonators or transducers in documents
5 concerning this technology, but each body actuates
6 several inkjets.

7 In the description of the prior art contained in
8 European patent EP 0 449 929 B1 it is recalled in col. 1,
9 lines 24-25 and 54-58 that, for chambers comprising
10 several jets, each nozzle is positioned facing either its
11 own acoustic vibration generator or a section of a
12 longitudinal acoustic generator whose measurements extend
13 parallel to the line formed by the jet-nozzle assembly.
14 The acoustic generator is supplied with sufficient power
15 to print a vibration with ink in a direction parallel to
16 the jet. The patent then points out in col. 2, lines 1-8
17 that this configuration of the vibration generator
18 relative to the nozzle plate is not indispensable
19 provided certain conditions of resonance are met. If the
20 conditions of resonance are complied with a single
21 acoustic generator can stimulate the ink passing through
22 a line of nozzles or part of a line of nozzles that has a
23 length considerably greater parallel to the line of

1 nozzles than the size of the acoustic generator in the
2 same direction, for example 5 to 10 times larger. The
3 condition to be complied with is that the vibrating body
4 vibrates virtually only in a longitudinal mode and at a
5 resonance frequency that differs by -10% of the
6 excitation frequency of the natural resonance vibrations
7 in the ink of the cavity between the end of the body and
8 the nozzle plate, the width of the body being smaller
9 than the length of the series of nozzles or the part of
10 the series of nozzles associated with said body.

11 In this patent the lateral walls of the ink chamber
12 have a cross-section perpendicular to the line of nozzles
13 disposed in a V shape. The tip of the V is turned towards
14 the line of nozzles. The section of chamber comprising
15 the V-shaped walls may be changed to enable the height of
16 the V to be varied depending on the density of the ink
17 and therefore the speed of the sound in the ink used.

18 Patent application WO 98 51503 also describes an
19 ink-drop generator for an inkjet printer with the
20 following characteristics: the lateral walls of a cavity
21 containing the ink consist of interior and exterior
22 walls. The resistance component of the acoustic impedance
23 of the external walls is such that the external walls

1 passively dampen the vibrations of the interior walls by
2 dispersing the vibrations. The reactive component of the
3 acoustic impedance of the external walls is such that the
4 external walls actively inhibit the vibrations of the
5 internal walls, said external walls thus ensuring that
6 each inkjet sprays drops of ink at the same predetermined
7 distance from each respective nozzle. This type of
8 configuration is used to prevent the nozzle bearing plate
9 from bending in a direction parallel to the inkjet when
10 the printer is used.

11 The present applicant has filed European patent
12 application EP 0 532 406 A1 concerning multijet modules
13 and the juxtaposition of several modules positioned side-
14 by-side to obtain a large printing width. Much of the
15 detailed description of the embodiment given below
16 repeats the description of the above-mentioned
17 application, particularly everything that relates to the
18 mechanical fastening of print modules to a module
19 assembly beam.

20
21 Brief description of the invention

22 As in the examples of embodiments in European patent
23 applications EP 449 929 B1 or EP 0 532 406 A1 referred to

1 above, the invention relates to a multijet print head,
2 i.e. a head in which a cavity containing pressurized ink
3 delivers several jets that are divided into drops by a
4 single resonator for said cavity. As in the embodiment
5 described in European patent application EP 0 532 406 A1,
6 the invention also relates to a print head capable of
7 being mounted such that it is aligned with other heads to
8 constitute a print assembly comprising a large number of
9 jets equidistant from one another capable of
10 simultaneously printing a wide band, for example two or
11 more metres.

12 The multijet cavities of the prior art described,
13 for example, in patent applications WO 98/51503 or EP 0
14 449 929 B1 referred to above, enable a single resonator
15 to actuate several jets. However, the end jets, i.e.
16 those leaving the first and last nozzles of the cavity,
17 spray irregularly, produce distorted drops or are formed
18 at variable distances when said end jets are too close to
19 the walls of the cavity.

20 The inventor of the present invention has used
21 digital simulations to improve the quality of the end
22 jets, for example by using a particular contour of the
23 lateral wall at the nozzle plate, i.e. where said lateral

1 wall is secant to the nozzle plate. Another factor that
2 affects the quality of the end jets is the angle formed
3 by the lateral wall of the cavity with the nozzle plate.
4 The angle is preferably 90° along the entire contour of
5 the lateral wall.

6 The relation between the vibrating surface of the
7 resonator and the surface of the nozzle plate should also
8 be taken into consideration. The relation between the
9 surfaces should preferably be approximately 1, for
10 example between $3/4$ and $4/3$. The shape of the
11 transitional surface between a resonator housing and the
12 cavity also plays a role. Finally, the relation of the
13 cavity measurements is also important. Each of the
14 factors mentioned above provides an improvement and the
15 combination of all or some of the factors enables the
16 spray quality of the end jets to be indistinguishable
17 from the quality obtained with the central jets.

18 It becomes possible to position the end-nozzles very
19 close to the intersection of the lateral wall of the
20 cavity with the axial line joining the nozzles. Under
21 these conditions, even though the distance between
22 consecutive nozzles may be small, it remains possible to
23 create an alignment of several cavities in which all the

1 nozzles are equidistant despite the thickness of the wall
2 separating two consecutive cavities of the same head or
3 two consecutive print heads.

4 Compared to known embodiments, the present invention
5 also relates to an ink-drop generator suitable for a wide
6 range of inks that does not require the drop generators
7 to be modified and that can be produced in materials
8 capable of withstanding temperatures to which print heads
9 may be exposed in an industrial environment.

10 To achieve all these aims, the invention relates to
11 an ink-drop generator for an inkjet printer in which an
12 inkjet is sprayed in drops, said generator particularly
13 comprising:

- 14 - a generator body,
- 15 - at least one acoustic wave generator with a body
16 elongated in an axial direction to the inkjets, each
17 generator having a vibrating surface perpendicular to the
18 axial direction of the jets, at least one section
19 comprising the vibrating surface of each acoustic
20 generator being housed in a housing of the drop-generator
21 body,
- 22 - at least one resonance cavity intended to contain
23 ink, the first section only of each cavity possibly being

1 constituted in a main section of said body constituting
2 the main body of the generator and, in this
3 configuration, a second section in a continuation of said
4 main body of the generator connected to be leaktight to
5 the main body of the generator, each cavity having an ink
6 feed and an ink-feed aperture, each cavity being
7 particularly defined by a nozzle plate and a lateral wall
8 secant to the nozzle plate, the intersection of the
9 lateral wall and the nozzle plate defining a first
10 contour line of the lateral wall, the nozzle plate
11 comprising a plurality of nozzles aligned along an axial
12 direction of the nozzles perpendicular to the axial
13 direction of the jets, the axial direction of the jets
14 and the axial line of the nozzles defining a plane of the
15 jets,

16 - a generator characterized in that the lateral wall
17 of each resonance cavity is secant to the nozzle plate
18 perpendicular to said nozzle plate along the entire first
19 contour line of said wall, the first contour line being
20 formed by two equal segments that are parallel to one
21 another and the axial direction of the nozzles, each
22 segment having two ends: a first and a second end, the
23 two first ends of each segment being connected by a first

1 curved line and the two second ends of each segment being
2 connected by a second curved line.

3 The lateral surface of the cavity therefore consists
4 of two plane walls parallel to one another and, at the
5 axial line of the nozzles, one of the walls containing
6 one of the segments and the other, the other segment, and
7 two curved connecting walls each containing one of the
8 contour curves.

9 In one embodiment the connecting curved lines of the
10 segment ends are concave towards the inside of the
11 cavity. In general, in order to facilitate manufacture
12 the curved lines are constituted by semicircles the
13 diameter of which is the space between the two segments.
14 Preferably, in order to facilitate a preferred vibration
15 mode in the fluid the largest measurement 1 of the first
16 contour of the cavity lies along the axial line of the
17 nozzles, the distance between the two segments is
18 approximately $1/4$ and the height of the lateral wall of
19 the cavity is between $1/2$ and $31/4$, preferably
20 approximately $51/8$. To enable the vibrations produced by
21 the acoustic-wave generator to be transmitted to the ink
22 contained in the cavity it is necessary to connect the
23 acoustic-wave generator housing to the cavity. The

1 connection is achieved by a hollow connector section
2 defined by a lateral connector surface. Said connector
3 surface is intended to connect, for example, a
4 cylindrical shape with a circular base, the diameter of
5 which is the diameter of the acoustic-wave generator, to
6 a cylindrical shape with a more or less flattened
7 rectangular base that is the shape of the lateral surface
8 of the ink cavity. As described above, the space between
9 the two walls of the largest surfaces of the cavity is
10 preferably equal to $1/4$. The connector surface is
11 preferably obtained as follows: to create the first
12 section of the surface the cylindrical surface with a
13 circular base, the diameter of which is between $1/2$ and
14 $31/4$ of the acoustic-wave generator, is extended over the
15 section of its periphery that lies between the two planes
16 defined by the largest plane walls of the cavity
17 separated by a distance of $1/4$.

18 Each of the largest walls and/or a continuation of
19 each wall is also hollowed to obtain a hollow the
20 periphery of which is defined by a curved line in the
21 plane of said wall and part of a circle the diameter of
22 which is equal to the diameter of the acoustic-wave

1 generator, said circle being located in a plane
2 perpendicular to the plane wall of the cavity.

3 The base of the hollow section, which is defined as
4 described above, may be a conical surface, for example,
5 to obtain a progressive junction between the generator
6 housing and the resonance cavity. This junction forms an
7 opening with a more or less rectangular cross-section
8 between the resonator housing and the resonance cavity.
9 The junction of the walls between the resonator housing
10 and the cavity is achieved progressively.

Brief description of the drawings

11 An example of an embodiment of the invention will
12 now be described with reference to the attached drawings
13 where:

14 - figure 1 is an exploded perspective view of an
15 example of an embodiment of the mechanical parts of a
16 print head, the said parts comprising in particular the
17 ink-drop generator body and an ink distributor /
18 collector;

19 - figure 2 is a longitudinal cross-section along the
20 plane of the ink-drop generator body and its
21 continuation;

1 - figure 3 is a section through the assembled body
2 with its continuation in a plane perpendicular to that of
3 the jets and parallel to the nozzle plate;

4 - figure 4 is a transverse cross-section along a
5 plane perpendicular to that of the jets and that of the
6 nozzle plate of the ink-drop generator body and its
7 continuation;

8 - figures 5 are in three parts, A, B and C; these
9 three parts of the figure show the shapes of the contours
10 of the intersection of the connection surface between the
11 housing of the sound wave generator and the cavity, the
12 said sections being along planes parallel to the nozzle
13 plate;

14 - figure 6 is a cross-section through the generator
15 body along line E-E of figure 2;

16 - figure 7 shows a perspective view of part of a
17 printer comprising an alignment of print heads comprising
18 ink-drop generators of the invention;

19 - figures 8 and 9 show schematic views of cross-
20 section of the part located behind a multijet print
21 module fitted on a supporting beam of a plurality of
22 modules;

1 - figure 8 particularly shows a detailed view of the
2 ink feeding pipes;

3 - figure 9 particularly shows a detailed view of the
4 ink drainage and recovery pipes;

5 - figure 10 shows part of a printer designed to show
6 the shape of the feeding pipes of the various ink
7 generators;

8 - figure 11 shows part of a printer comprising
9 several alignments of print heads arranged in series.

10 Figure 1 is an exploded perspective view of an
11 assembly of mechanical parts composing part of an ink-
12 drop generator 33 of the invention. It will be seen below
13 that the generator 33 comprises a body 133, an ink
14 distributor / collector 29 and an ink-drop deflection
15 assembly 32. In the part discussed here relative to
16 figure 1 the body 133 and distributor / collector 29 will
17 be described.

18 Body 133 comprises a dual body 1 forming main body 1
19 and a continuation 2. Dual body 1 comprises a section
20 with two cavities 6. Each cavity 6 is partly composed of
21 a hollow in dual body 1 and partly of a hollow in
22 continuation 2 of dual body 1. Continuation 2 is
23 connected to dual body 1 by means of a sealed connection.

1 The continuation 2 of dual body 1 is mechanically
2 composed of a mechanical assembly of three parts, a
3 housing 4 of a cavity part, a thin strip 3 bearing
4 calibrated holes 36 forming nozzles and a reinforcement
5 plate 5. The reinforcement plate 5 and strip 3 are
6 fastened by means of a sealed connection, known per se,
7 for example welding, to a base located outside housing 4
8 of some of the cavities 6. Holes in part 5 and the base
9 of part 4 allow jets of ink to pass from inside cavity 6
10 through nozzles 36. This embodiment of the nozzle-plate,
11 known per se, makes it possible very accurately to
12 calibrate the nozzles, for example by laser-cutting thin
13 strip 3 to form a clean, neat hole with a diameter of a
14 few tens of μm . In the rest of the present text any
15 reference to nozzle plate 39 is understood to refer to an
16 assembly 39 comprising housing base 4, strip 3 and
17 reinforcement 5.

18 Body 133 is divided into two sections, dual body 1
19 forming the main body and continuation 2 of the body for
20 machining purposes. The opening in body 133 allows
21 machining of the upper section of cavities 6 using a bit
22 that machines the bottom of dual body 1 and that in the

1 lower section of the same cavities via the top of
2 continuation 2 of main body 1.

3 Other than the screws, the leaktightness,
4 positioning and fastening means of main body 1 and its
5 continuation 2 are shown in the drawings but not
6 commented upon as they are known per se.

7 A description of a cavity 6 will now be given with
8 reference to figures 2 and 3. Figure 2 is a cross-section
9 along the plane of the jets of main body 1 and its
10 continuation 2 mounted together. Figure 3 shows a cross-
11 section through body 133 along plane C-C of figure 2
12 close to the nozzle plate and parallel to the said nozzle
13 plate.

14 A cavity 6 has the general shape of a rectangular
15 parallelepiped of length 1, width more or less $1/4$ and
16 height somewhere between $1/2$ and $3 1/4$ but preferably
17 $5 1/8$. As explained above, these measurements are designed
18 to encourage vibrations propagating along a plane wave
19 parallel to nozzle plate 39. The shape of this cavity
20 will now be explained in more detail with reference to
21 figure 3. As stated above, this figure shows a section
22 through a plane parallel to the nozzle plate located a
23 very short distance from the nozzle plate. The contour of

1 this cavity consists of two planar segments 7, 8 that are
2 generally parallel to one another and located at an
3 approximate distance of 1/4 from one another. A side of
4 each segment ~~Said segments 7, 8 are~~ is illustrated in
5 figure 3 as the trace in the cross-sectional plane of
6 ~~mutually the~~ parallel segments 7, 8 that define an inner
7 periphery of a portion of the cavity 6. ~~flat walls 7, 8~~
8 ~~that will be referred to hereafter as the large walls of~~
9 ~~cavity 6.~~ Said ~~large walls~~ segments 7, 8 are connected by
10 ~~semi-circles~~ arcuate planar portions 9, 10 a side of each
11 arcuate planar portion 9,10 being illustrated in figure 3
12 ~~as that are~~ the trace in the cross-section plane of
13 ~~eylindrical walls~~ the arcuate planar portions 9, 10. It
14 will be seen from this drawing that cavity 6 is not
15 altogether parallelepiped-shaped since a portion of its
16 inner periphery includes arcuate formations causing the
17 cavity 6 ~~two of its walls 9 and 10 consist of concave~~
18 ~~walls turning into the cavity having in this case to have~~
19 the shape of half-cylinders with circular bases. As can
20 be seen from figure 2 or figure 4, which is a cross-
21 section through body 133 along line B-B, shown in figure
22 2, of a cavity, that also passes through the axis of a
23 jet, ~~lateral walls~~ arcuate planar portions 9, 10 and

1 segments 7, 8 of the cavity 6 are joined perpendicularly
2 to nozzle plate 39. This shape makes it possible to avoid
3 upward reflections of waves on the walls induced by the
4 V-shaped form of these walls as described in the WO
5 patent application cited above in the description of the
6 prior art. This shape therefore makes it possible to
7 obtain more regular vibration of the ink in the cavity 6.

8 In each cavity the apertures 11, shown particularly
9 in figure 2, provide the cavity with a supply of
10 pressurized ink. The ink flows through the nozzles 36
11 once the printer is operating. During jet startup,
12 shutdown or maintenance, the ink may also be supplied in
13 large quantities via aperture 12. This aperture has a
14 cross-section greater than the sum of the cross-sections
15 of the two ink-supply apertures 11.

16 The direction of the ink feeding pipes 11 is in the
17 plane of the preferred vibration mode, perpendicular to
18 the direction of the jets in order to minimise vibration
19 disturbance. With the same end in mind they are also
20 directed more or less along the smallest measurement $1/4$
21 of the cavity in order to minimise coupling with the main
22 mode of interference vibration, which is that oriented
23 along the largest measurement 1 of the cavity.

1 The two feed apertures 11 are located symmetrically
2 relative to a central plane of cavity 6 perpendicular to
3 the plane of the jets, and immediately below upper
4 surfaces 107, 108 of the cavity. Ink outlet aperture 12
5 is located in a housing 13 of ~~shaker~~ acoustic wave
6 generator 14. The ink supplied via apertures 11 is
7 intended to keep the cavity 6 filled and under pressure
8 while the ink leaves via the nozzles 36. The ink outlet
9 aperture 12 is used during startup, shutdown and
10 hydraulic maintenance phases of the print head. The
11 relative disposition and cross-sections of ink inlet
12 aperture 11 and ink outlet aperture 12 are optimized to
13 ensure uniform distribution of the ink to the nozzles, so
14 as to ensure that the ink in the cavity is not disturbed
15 by the ink-flow pulsations coming from the ink circuit,
16 to ensure that the ink in the cavity is replaced rapidly
17 (drainage), and to eliminate any air bubbles in the
18 cavity by ensuring that there is a high flow-rate of
19 liquid during hydraulic maintenance sequences. The body
20 also contains housings 13 each provided for an acoustic
21 wave generator 14 already known per se that has the basic
22 shape of a cylinder 15 ending in a surface 16 that is
23 parallel to the plane of the nozzles, said surface 16

1 constituting the vibrating surface of the acoustic wave
2 generator 14. The section of the housing 13 of the
3 acoustic wave generator 14 closest to the cavity has the
4 shape of a cylinder 17.

5 In figures 2 and 4 the acoustic wave generator 14 is
6 shown in dotted lines, firstly in a position close to its
7 assembled position, and secondly once in its assembled
8 position. In the assembled position the contour of the
9 acoustic wave generator 14 is practically identical in
10 figures 2 and 4 with that of the housing of the generator
11 14. In the drawings, particularly figures 2 and 4, the
12 housing of the acoustic wave generator 14 is located
13 above cavity 6. This "above" position is in no way
14 compulsory in practice. However, the terms "above" and
15 "below" are used as a convenient spatial reference to
16 describe the position of components relative to one
17 another. In the example shown, the cylinder of the
18 acoustic wave generator 14 is of diameter $1/2$, i.e. half
19 the length of cavity 6 and its axis lies both in the
20 plane of the jets and equidistant between the ends of
21 cavity 6. In operation, the vibrating surface 16 of
22 generator 14 is located level with the upper section of
23 the cavity 6. This arrangement is in no way compulsory

1 and this surface may be disposed slightly higher in the
2 housing 13 of the acoustic wave generator 14. Given the
3 shape of the acoustic chamber and the shape of the
4 housing of generator 14, in order for the acoustic waves
5 to be transmitted efficiently and in a preferred
6 vibration mode through the ink in cavity 6, it is
7 necessary to provide a connection 18 between housing 13
8 of acoustic wave generator 14 and cavity 6. This
9 connection 18, which consists of a hollow in the ~~flat~~
10 walls segments 7, 8, will now be described.

11 It should first be noted that in terms of the width
12 of cavity 6 the connection is provided by the
13 continuation of the cylindrical surface of housing 13 of
14 acoustic wave generator 14. This point will be explained
15 in greater detail below with reference to figure 5A.

16 Figure 5A shows the shape of the cross-section of
17 cavity 6 as a plane parallel to the plate 39 carrying the
18 nozzles 36. The projection on the cross-section plane of
19 cylinder 17 forming the housing of acoustic wave
20 generator 14 is also shown in dotted lines on a section
21 outside cavity 6 and in unbroken lines inside cavity 6.
22 The centre of the circle representing this projection is
23 located on the longitudinal axial line of cavity 6

1 equidistant between the two ends of this cavity. For the
2 sections of the connection located between the two ~~planes~~
3 ~~defined by each of plane surfaces~~ planar segments 7 and 8
4 of cavity 6 ~~comprising segments 7 and 8~~ shown in figure
5 5A, the connection surface ~~consists~~ includes as shown in
6 part A of continuations 19 and 20, shown by unbroken
7 lines, of the cylindrical section 17 of the housing 13 of
8 acoustic wave generator 14. In this way, looking at
9 connection 18 along an axial line of a jet, it will be
10 seen to have a shape whose projection onto the cross-
11 section plane shown in figure 5A will now be explained.

12 This opening is composed of a closed cylindrical
13 surface comprising, on the one hand, continuations ~~parts~~
14 19 and 20 of the cylindrical surface and, on the other,
15 the flat parts of the surfaces of the planes containing
16 segments 7 and 8 lying between the ends of said ~~parts~~
17 continuations 19 and 20 of the cylinders. The shape of
18 that section of the lateral surface of connection 18 that
19 lies between ~~parts~~ connection 19 and 20 of the
20 cylindrical surface will now be explained.

21 In order to define this shape, figure 5B shows a
22 cross-section through the wall of ~~housing~~ connection 18
23 in a plane parallel to the nozzle plate located between a

1 low end section and a high end section of connection 18.
2 The cross-section of this connection consists of a line
3 comprising, in order, an end of ~~cylindrical wall~~
4 continuation 19, a straight section 22 that is part of
5 segment 7, followed by a curved section 21, and finally
6 another section 23 of segment 7, an end of ~~cylindrical~~
7 ~~wall~~ continuation 20 and sections 23', 21', 22' that are
8 respectively symmetrical with sections 23, 21, 22
9 relative to a longitudinal axis XX' of the cavity. We
10 will now consider the variations in the length of said
11 curved section 21 between the low end section of the wall
12 and the high end section. In the low end section of
13 connection 18 the length of curved section 21, shown in
14 part A of figure 5, is nil such that the perimeter of the
15 section is composed of sections of ~~eircles~~ continuations
16 19 and 20, ~~parts~~ sections 22, 23 of segment 7 joining the
17 ends of ~~eircles~~ continuations 19 and 20 and ~~parts~~
18 sections 22', 23' of segment 8 joining the ends of said
19 ~~parts~~ continuations 19, 20. When the cross-section plane
20 located between the low end sections and the high end
21 sections approaches the high end section the measurements
22 of ~~segments~~ sections 22, 23 located between curved
23 section 21 and each of ~~eircles~~ continuations 19, 20

1 respectively diminish and the length of curve section 21
2 increases. As the high end section as shown in part C of
3 figure 5 is reached the length of ~~segments~~ sections 22
4 and 23 is nil and curve section 21 consists of a circular
5 section ~~locating in the continuation of circles~~ forming a
6 continuous arcuate portion extending between
7 continuations 19 and 20.

8 Naturally if housing 13 and generator 14 were not
9 circular cylinders but had a different shape, curve
10 section 21 at the top would have the shape resulting from
11 an intersection of this shape with a plane parallel to
12 the nozzle plate. In the example described the
13 intersection of high end section of connection 18 with a
14 plane parallel to nozzle plate 39 consists of a circular
15 closed line whose diameter is equal to the diameter of
16 housing 13 of acoustic wave generator 14, for example
17 1/2. The perimeter of this line is the perimeter of the
18 circle. For an intermediary plane between the high end
19 section and the low end section the perimeter of the
20 straight cross-section of connection 18 by a plane
21 parallel to nozzle plate 39 is formed ~~one~~ on the one hand
22 by ~~sections~~ continuations 19, 20 of the circle, by ~~parts~~
23 sections 22, 23 of segment 7, by a curved section 21 by

1 parts 22', 23' of segment 8 and by a curved section 21'.
2 The perimeter of this intermediate cross-section is
3 therefore smaller than the diameter of the circle located
4 at the high end section. Similarly, coming to the low end
5 part, the cross-section of connection 18 by a plane
6 parallel to nozzle plate 39 has the shape shown in part
7 A, i.e. two sections 19, 20 of a circle and two ~~sections~~
8 continuations of segments 7 and 8 located between said
9 two sections of ~~circles~~ continuations 19, 20. The
10 perimeter of the low end part, shown in part A, is
11 therefore smaller than the perimeter of the intermediate
12 lower-part shown in part B. Therefore the shape of
13 connection 18 can be characterized by saying that the
14 perimeter of its cross-section by a plane parallel to
15 nozzle plate 39 reduces the further the plane of
16 intersection is from the upper limit and approaches the
17 lower limit.

18 It will also be noted that the ends of each of
19 ~~curves~~ sections 21, 21' are located facing one another
20 and thus separated from one another by a distance between
21 segments 7 and 8 of the first contour. In order for good
22 plane propagation of the acoustic waves to occur, the
23 walls of cavity 6 and connection 18 need to have

1 rotational symmetry, i.e. symmetry relative to an axis or
2 to two perpendicular planes passing through the said
3 axis.

4 In one simple embodiment, part of connection 18 is
5 made using a conical drill bit with an angle at its tip
6 of, for example, 90°. When the bit is conical the
7 different ~~curves~~ sections 21 are segments of circles of
8 nil diameter at the lower end section and a diameter
9 equal to that of housing 13 of the acoustic wave
10 generator 14. This embodiment is shown in figures 2 and
11 4. In figure 2 the intersection of the cone with the
12 plane of ~~surface~~ segment 7 of the cavity results in a
13 segment 24 of a hyperbola while figure 4, in which the
14 cross-section is along section B-B, i.e. more or less
15 along the axis of housing 13 of acoustic wave generator
16 14, the intersection has the shape of two 90° segments
17 26. In this example, moreover, the low end section of
18 housing 13 coincides with the high end section of cavity
19 6 and thus a low end section 25 of connection 18 is
20 positioned at a distance from the top of cavity 6
21 slightly less than half the diameter of the cylindrical
22 section of housing 13 of ~~\$\$acoustic~~ acoustic wave
23 generator 14. \$\$

1 Another important characteristic of the invention
2 will now be explained. As was seen above, because the
3 ~~lateral walls~~ segments 7, 8, and arcuate planar portions
4 9, 10 of the cavity are perpendicular to the nozzle plate
5 39 at the level of said nozzle plate 39 and that the
6 section of connection 18 between the lower surface 16 of
7 ~~resonator~~ acoustic wave generator 14 and cavity 6 is
8 created progressively, a plane wave perpendicular to the
9 axis of housing 13 propagates in cavity 6. As this wave
10 is plane, no problems are created due to boundary
11 effects. Consequently a nozzle 361, 362 may be positioned
12 very close to one of ~~walls~~ arcuate planar portions 9, 10
13 without its operation being affected. For example, it
14 will be seen from figures 2 and 3 that an end-nozzle 361
15 is located very close to the ~~outer wall~~ arcuate planar
16 portion 10 of cavity 6. Similarly it will be seen that an
17 end-nozzle 362 is located very close to a ~~wall~~ the
18 arcuate planar portion 9 separating two identical
19 cavities of body 133. The closeness of nozzle 361 to the
20 ~~outer wall~~ arcuate planar portion 10 allows the axis of
21 the nozzle to be at a distance less than half the
22 interval between two consecutive nozzles of the cavity
23 even if said interval is small. Similarly the distance

1 between end-nozzle 362 of ~~wall~~ arcuate planar portion 9
2 between two cavities 6 allows the distance between this
3 nozzle 362 and the next consecutive nozzle located in the
4 other cavity of body 133 to be less than the distance
5 between two consecutive nozzles in a single cavity. Hence
6 the interval between consecutive nozzles of all the
7 nozzles in the two cavities remains equal, even when it
8 is small. Moreover, due to the fact that the distance
9 between one end-nozzle and the outer surface of the ~~wall~~
10 portion where it intersects with the axis of the nozzles
11 is less than half the interval between two nozzles, it
12 becomes possible to place side by side two modules that
13 are, for example, identical or have the same
14 characteristic that the closeness of the nozzle of one
15 cavity relative to the outer surface of the body
16 containing ~~the~~ said cavity, without the interval between
17 two consecutive nozzles of the resulting assembly being
18 modified.

19 To take the best advantage of this fact without the
20 tolerances of an assembly of different bodies 133
21 resulting from the accumulated effect of the measurement
22 tolerances on each body, each body is fitted with
23 positioning pins 124 that cooperate in a way known per se

1 with positioning holes on a support beam 28 bearing the
2 alignment of the bodies. Clearly the effect would be the
3 same if the pins were on the alignment beam and the
4 bodies fitted with positioning holes.

5 In the example explained here and shown particularly
6 in figure 1, the positioning pins 124 are not fastened
7 directly onto main body 1. Body 1 is fastened onto an ink
8 distributor / collector 29. The distributor is an
9 intermediate part used to connect body 133 to the ink
10 circuit. For this purpose it has as many ink collection
11 gutters 34 as there are nozzles and ink inlets and
12 outlets known per se to maintain cavity 6 under pressure.
13 Part 29 is connected to body 133 by any fastening means
14 and is positioned by positioning means, for example by
15 continuations of the pins 124 fitting into the holes (not
16 shown) in body 133.

17 It will be seen that in the embodiment described
18 above the surface of nozzle plate 39 is $\frac{l^2}{16} \left(3 + \frac{\pi}{4} \right)$ and that
19 the vibrating surface 16 of the resonator is $\frac{\pi d^2}{16}$ such
20 that the relation of the values of these two surfaces is
21 $\left(\frac{3}{\pi} + \frac{1}{4} \right)$ or approximately 1.15.

1 The location of the ink inlet and outlet apertures
2 will now be described with reference to figures 2 and 6.
3 Figure 6 is a cross-section through dual body 1 at
4 apertures 11 and 12 in a plane parallel to nozzle plate
5 39.

6 As shown in figure 2, the ink inlet apertures 11 are
7 each located at one end of cavity 6 more or less directly
8 above end-nozzles 361, 362 respectively.

9 Since the diameter of the nozzles is very small
10 (approximately $50\mu\text{m}$), the rate of ink flowing through
11 them is very slight. It follows that the ink-flow
12 supplied to the nozzles is also very small. The cross-
13 section of ink inlet apertures 11 and ink outlet
14 apertures 12 is set at a measurement considerably greater
15 than the diameter of the nozzles such that the speed at
16 which the ink still in the cavity travels is very slight.
17 The ink is therefore subject to the vibrations of the
18 transducer while it is virtually static.

19 The disposition of the ink inlet apertures 11 on the
20 top ends of cavity 6 and immediately beneath upper
21 surfaces 107, 108 respectively of cavity 6, which at this
22 point mask the propagation of acoustic waves, limit the
23 disturbance of vibrations by the ink-flow.

1 During maintenance operations the ink outlet occurs
2 higher through an aperture 12 (shown in figure 2) located
3 in the cylindrical section 15 of housing 13 of acoustic
4 wave generator 14. The ink flows towards outlet aperture
5 12 from cavity 6 through a clearance between the
6 cylindrical section 15 and ~~resonator~~ acoustic wave
7 generator 14. The use of a single outlet aperture 12
8 eliminates areas of static fluid and optimizes drainage
9 of the ink cavity. Finally, in normal operation the
10 solenoid valves controlling the print head prevent ink
11 from flowing through outlet aperture 12; the ink around
12 this aperture is therefore static. It also acts as a
13 lubricant and vibration insulator for ~~resonator~~ the
14 acoustic wave generator 14.

15 Figure 6 shows ink pipes 37. The outermost sections
16 of these pipes join curved surfaces 9, 10 such that they
17 are tangential in order to optimise the drainage of the
18 cavity. The two pipes 37 are symmetrical to one another
19 relative to a perpendicular plane of the jet plane. They
20 open into a distribution throat 88 located between dual
21 body 1 and collector / distributor 29.

1 The assembly of generators or ink print modules 33
2 that each comprise a body 133 and an ink collector is
3 described below with reference to figures 7-9.

4 An example of this kind of module mounted on a beam
5 28 is shown in figure 7. Figure 7 is a view showing a
6 printing device comprising an assembly of eight print
7 modules 140 of $m = 8$ print jets 27 that form a continuous
8 row of 64 regularly spaced print jets. The eight print
9 modules are mounted adjacent to one another on a
10 supporting beam 28 common to all the modules. Each print
11 module comprises:

12 - a collector / distributor 29
13 - a multijet deflector assembly 32
14 - a body 133
15 - the collector / distributor, which is a one-piece
16 body 29 comprising gutters 34 for collecting the non-
17 deflected drops of each jet, supports body 133 which is
18 capable of delivering 8 inkjets through 8 nozzles 36; the
19 eight inkjets are regularly spaced in a plane parallel to
20 beam 28;

21 - multijet deflector assembly 32 is shown in two
22 positions: in the low, or working position on the modules
23 located the furthest to the left of figure 7 and in the

1 high, or maintenance position on the modules located the
2 furthest to the right. The function of this type of
3 deflector assembly and its construction are known in
4 themselves. They will only therefore be described briefly
5 below. When each jet of liquid leaves nozzles 36 it
6 breaks up into micro droplets and passes through multijet
7 deflector assembly 32 where certain drops are
8 electrically charged by charge electrodes then deflected
9 from their initial trajectory towards gutter 34 by
10 deflecting electrodes, said deflecting and charge
11 electrodes belonging to deflector assembly 32, to create
12 an impact on a printing substrate that scrolls in front
13 of the printing module. This type of multijet deflector
14 assembly 32 to deflect $m = 8$ inkjets is described, for
15 example, described in French patent application No. 91
16 05475 filed by the present applicant on 3 May 1991.

17 An actuating part 31 that rotates multijet deflector
18 assembly 32 around an axis 49 is constructed as part of
19 supporting beam 28.

20 It will be seen in reference to figures 8 and 9 that
21 the side of supporting beam 28 opposite that bearing
22 collector 29 of each print module is associated with a
23 single part 30 that creates, in combination with said

1 beam 28, a tank 62 for collecting or draining the ink
2 from the collector gutters of the eight print modules
3 and, in combination with a single plate 110, a single
4 cavity 111 for distributing the ink to the eight devices
5 33 for generating the eight inkjets. Support beam 28 has
6 internal pipes that connect, on the one hand, collector
7 tank 62 and, on the other, gutters 34 of generator
8 devices 33 mounted on supporting beam 28 and the internal
9 supply pipes.

10 It should be noted that figures 8 and 9 are
11 essentially schematic cross-sections to support the
12 description and are not actual cross-sections of the
13 device. It is for this reason that pipes in the figures
14 are not always in the cross-section plane but in the
15 parallel planes. The schematic cross-section of figure 8
16 is mainly of a plane of the feed pipes of a print module
17 33 and a plane of ink-collector pipes undirected towards
18 a printing substrate from gutters 34. The pipes used for
19 ink collection are not necessarily in the same plane as
20 those used for the supply.

21 Similarly, figure 9 mainly shows the plane of the
22 ink drainage and collection pipes but the pipes relative

1 to these two functions are not necessarily in the same
2 plane.

3 As described above, body 133 is supplied with ink
4 through pipes 37 pierced in body 133 and a collector
5 throat 88 between body 133 and collector 29. Throat 88
6 communicates with the rear of collector 29 via a hole
7 pierced through said collector, as shown in figure 1 by
8 an arrow. Similarly, drainage opening 12 communicates
9 with the rear of collector 29 via pipes pierced in body
10 133 and collector 29. Gutters 34 for collecting unused
11 ink drops from a jet, i.e., non-deflected drops, provided
12 in the lower section of collector 29 communicate with the
13 rear section of collector 29 via an internal pipe of said
14 collector 29. The eight internal pipes open into a
15 suction cavity of collector 29.

16 Figures 8 and 9 show the workings at the rear of
17 collector 29 in terms of the ink circuits.

18 The ink supply circuit of each print module will now
19 be described with reference to figure 8. This figure is a
20 schematic transversal cross-section through a supporting
21 beam 28 of an assembly of modules and components on the
22 rear section of said beam 28. A part 30 is assembled onto
23 beam 28 by bolts and impervious seals (not shown). These

1 bolts are also used to assemble a rear plate 110 to the
2 rear of part 30.

3 Ink is distributed to all cavities 6 of the eight
4 modules by a pressurized distributor 111 created on the
5 rear surface of part 110. The distributor communicates
6 with pipes 38 pierced through beam 28 via pipes that are
7 preferably rigid, such as pipe 144 shown in figure 8 and
8 solenoid valves 86 called feeding valves. In figure 8 a
9 single connector pipe 144 between distributor 111 and a
10 single solenoid valve 86 are shown. In fact there are as
11 many pipes, solenoid valves 86 and pipes 38 as print
12 modules.

13 Pressurized cavity 111 communicates with ink
14 pressurizing means (not shown) via a connector 69.

15 A tank 62, shown in figures 8 and 9, is created by a
16 first cavity provided in beam 28 and a second cavity
17 provided in part 30. The collection and drainage circuit
18 will now be described with reference to figure 9.

19 Tank 62, called the collector or drainage tank, is
20 connected to a solenoid valve 89, called a drainage
21 valve, via a pipe 63 of part 30, a throat 64 between
22 parts 30 and 110, a pipe 65 pierced in part 110, an
23 external pipe 120, a pipe 92 of part 30, a throat 91

1 between parts 30 and 110 and a pipe 90 pierced in part
2 30. Said solenoid valve 89 is also connected to the rear
3 of collector 29 by a pipe 77. Said pipe 77 communicates
4 with opening 12 of cavity 6 through collector 29 and body
5 133. Tank 62 is common to all the print modules mounted
6 on beam 28, i.e. the eight modules shown in figure 7.
7 There is a pipe 77, 90, 65, 63, a throat 91, 92 and a
8 drainage solenoid valve 89 for each print module. Tank 62
9 also communicates with the collector gutters of
10 collectors 29 via pipes 59 pierced in beam 28. The single
11 tank 62 communicates with a suction pump (not shown) via
12 a single 73 pipe pierced through parts 30 and 110.

13 During printing the non-deflected ink from gutters
14 34 is permanently sucked and returned to the ink circuit.
15 In the drainage mode solenoid valves 89 are open and the
16 suction pump sucks ink from tank 62 collected from the
17 gutters and openings 12 of cavities 6.

18 Another aspect of the invention will now be
19 described with reference to figure 10 that shows a rear
20 perspective view of a supporting beam 28. As explained
21 above the rear surface of support 28 is associated with a
22 single part 30 that creates, in combination with said
23 beam 28, a collector or drainage tank 62 (figures 8, 9)

1 and, in combination with a plate 110, a cavity 111 for
2 distributing ink to the eight devices 33 for distributing
3 eight inkjets.

4 The aim of figure 10 is to show a characteristic of
5 pipes 141-144 that each supply an ink generator 33.

6 The aim of this characteristic is to ensure that the
7 pressure drops are identical in each pipe 141-144 joining
8 distribution cavity 111 to each generator 33,
9 irrespective of the position of the generator relative to
10 cavity 111.

11 To this end all pipes 141-144 are of the same
12 length.

13 Moreover, all the pipes include the same number of
14 elbows. The value of an elbow angle of a pipe is
15 identical on all the other pipes.

16 These characteristics of pipes will now be described
17 in detail in reference to figure 10. As this figure is a
18 semi-cross-section, only four pipes are visible. A pipe
19 that supplies four other pipes symmetrical to pipes 141-
20 144 relative to a plan perpendicular to beam 28 is not
21 shown.

22 Each connector pipe has a start end section 141a-
23 144a perpendicular to plate 110 and a finish end section

1 141b -144b also perpendicular to plate 110. The end
2 sections of a pipe, for example 144a, 144b, are connected
3 together by a central pipe section 144c parallel to plate
4 110. The length of this section varies depending on the
5 distance between the supply point of a generator 33 and
6 the starting point of cavity 111. The sums of the lengths
7 of sections a, b, c of each pipe 141-144 are equal. This
8 means, for example, that central section 141c of pipe 141
9 that supplies a generator 33 close to central supply
10 cavity 111 is shorter than central section 144c of pipe
11 144 that supplies a generator 33 further away from cavity
12 111. On the other hand end sections 141a, 141b of pipe
13 141 are longer than sections 144a, 144b of pipe 144.
14 Given the different configurations pipes 141-144 are
15 nevertheless equal in length. They each comprise two
16 connector elbows that are at right angles and with the
17 same radius of curvature. All the pipes are rigid, for
18 example metal, to enable them to retain their shape. In
19 the example of figure 10 it was not necessary to include
20 a section of S-shaped piping to absorb the dilations
21 although one could be provided depending on the
22 conditions of use of the printer assemblies. The position
23 of the S-shaped sections in the piping matters little, it

1 being essential however that they are identically shaped
2 and connected to the rest of the piping.

3 A printer of the invention comprises one or more
4 supporting beams 28 equipped with print heads 32 that
5 enable ink to be sprayed towards a printing substrate. In
6 principle when there are several beams each beam prints a
7 different colour ink such that a colour image is
8 produced. The advantage of a printer configured according
9 to the invention is that an entire width of the substrate
10 may be printed simultaneously. Under these conditions a
11 relative movement of the print heads and the substrate in
12 a parallel direction to beam 28 is no longer necessary
13 because the width that is printed simultaneously can be
14 adapted to the width of the substrate. The only remaining
15 movement is that of the head relative to the substrate in
16 a direction perpendicular to support beam 28. This may be
17 a continuous, rapid movement.

18 Figure 11 shows a printer provided with several
19 support beam assemblies 28 positioned parallel to one
20 another and printing the same substrate scrolling
21 perpendicular to the beams. Figure 11 is a schematic
22 perspective view of this type of configuration. A support
23 frame 150 holds a set of beam assemblies 28a, 28b, 28c.

1 Means (not shown) enable substrate 151 to scroll
2 under the inkjets of print modules or heads 14a of beam
3 28a, then 140b of beam 28b and 140c of beam 28c.

4 The beam 28a the furthest upstream relative to the
5 scrolling substrate periodically prints a reset mark, for
6 example on an edge of the substrate. Each downstream beam
7 28b, 28c is provided with a position sensor (not shown)
8 to detect these marks and enable the pixel data of the
9 line to be reset virtually continuously. Good
10 superimposition of colours is therefore obtained.